n , 0	characteristic constant for each family of sub
	stances
α_i	molecular polarizability of the component i, cm
	mol ⁻¹

а.	polynomial	coefficients	in er	14

- refractive indexes of A and D in eq 6 n_A, n_D
- volume fraction of the component A in eq 6 φ_{A}
- polynomial degree n
- density of the solution, g cm⁻³ D

Registry No. Methyl isobutyl ketone, 108-10-1; sec-butyl alcohol, 78-92-2; isobutyl alcohol, 78-83-1; n-butyl alcohol, 71-36-3.

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Thermodynamic Properties of Isobutane in the Critical Region

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For geothermal applications, a scaled fundamental equation has been formulated in order to represent and tabulate the thermodynamic properties of isobutane in the critical region. In the supercritical range, the surface joins smoothly with that of Waxman and Gallagher, to which it is a complement. The range of the surface is 405-438 K in temperature, 150-290 kg/m³ in density. The critical constants are T $_{\rm c}$ = 407.84 \pm 0.02 K, $ho_{\rm c}$ = $225.5 \pm 2 \text{ kg/m}^3$, $P_c = 3.629 \pm 0.002 \text{ MPa}$. Comparisons are made with the PVT data of Beattle et al., and of Waxman, and also with the formulations of Waxman and Gallagher, and of Goodwin and Havnes.

Introduction

Isobutane has been proposed as the working fluid in binary geothermal power cycles. In this application, the fluid would pass through the heat exchanger at a pressure exceeding the critical pressure ($P_c = 3.63$ MPa), while it is heated from ambient to supercritical temperatures ($T_c = 408$ K). The initial state of the fluid entering the turbine would be a supercritical pressure and temperature, while the density would be somewhat below the critical. The gas would then expand isentropically along a path that, preferably, should remain within the one-phase vapor region. Kestin and Khalifa (1, 2) pointed out that the then-existing formulations of the thermodynamic properties of isobutane were of insufficient reliability for design of an efficient cycle. The lack of reliability was due, to a considerable extent, to sparsity and inconsistency of the thermodynamic data. Since then, the situation has been remedied, at least to a good extent, by the acquisition of new data on the vapor pressure and on PVT of the vapor and supercritical phase by Waxman et al. (3-6), and on PVT of the liquid by Haynes (7). These new accurate data permitted Waxman et al. to select the bodies of reliable data.

It was decided to approach the formulation of the thermodynamic surface in two steps. Waxman and Gallagher (5, 6)

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adapted the free energy model developed by Haar and coworkers (8) to represent the thermodynamic properties of isobutane up to 40 MPa and from 250 to 700 K with the exclusion of a region around the critical point the size of which is

$$0.985 \le T_{c}/T \le 1.015$$
 i.e., $401.8 \le T \le 414$ K

 $0.7 \le \rho_{\rm c}/\rho \le 1.3$ i.e., 173.4 $\leq \rho \leq$ 322 kg/m³ (1)

The thermodynamic surface that we present here is valid in the range

$$405 \le T \le 438 \text{ K}$$

 $150 \le \rho \le 290 \text{ kg/m}^3$ (2)

and thus supplements the surface of Waxman et al. in most of the excluded range. The model that we use is that of revised and extended scaling, as developed according to the modern theory of critical phenomena (9). We have applied this model successfully to the thermodynamic properties of light and heavy water (10, 11) in the critical region. Here, however, we use a somewhat different approach toward determining the model parameters. We obtained most of our parameter values by a fit to the experimental PVT data of Beattle et al. (12, 13), which were recently validated by Waxman (6). There are a large number of PVT data in a very narrow temperature region, from 407.8 to 408.3 K, around the critical point; the only other data available in our range are on the 423.17 K isotherm. It is clear that temperature derivatives of the surface cannot be reliably taken if the surface is based on only two isotherms. We therefore supplemented the experimental data with PVT points generated from the surface of Waxman et al. in a range in which the surface is valid. This practice has yielded three benefits. It has helped pinpoint our surface, has ensured a smooth crossover to the analytic surface along most of the boundary, and has provided the entire analytic "background" for the caloric parameters, for which, in the case of isobutane, no experimental information is available.

The critical-point parameters incorporated in the scaled equation differ from those reported by Beattie et al. (12). If the critical parameters are freely adjusted in the fit to a scaled equation, the value of the critical temperature fails as much as

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0.3 K below that deduced by Beattie et al. from the same data. An independent experimental determination of the critical temperature of isobutane by one of us (J.M.H.L.S.) gave results very close to the low value of T_c that we deduced from Beattie's data. This is the value that we then used in the fit.

We present here tabulated values derived from our fundamental equation for the saturation properties and for pressure, energy, enthalpy, entropy, specific heats at constant pressure and volume, and speed of sound, along isotherms in the range given by eq 2.

Comparisons are presented with the experimental PVT data, with the analytic surface of Waxman et al., and with the coexistence curve of Goodwin and Haynes (7).

Scaled Fundamental Equation

Our fundamental equation involves a relationship between the intensive thermodynamic variables pressure P, chemical potential μ , and temperature T. Specifically we consider the reduced variables

$$\tilde{P} = \frac{P}{T} \frac{T_c}{P_c} \qquad \tilde{\mu} = \frac{\mu}{T} \frac{\rho_c T_c}{P_c} \qquad \tilde{T} = -T_c/T \qquad (3)$$

where P_c is the critical pressure, T_c the critical temperature, and ρ_c the critical density. The fundamental equation yields the thermodynamic potential \tilde{P} as a function of $\tilde{\mu}$ and \tilde{T} and has the form

$$\tilde{P} = \tilde{P}_{0}(T) + \Delta \tilde{\mu} + \tilde{P}_{11} \Delta \tilde{\mu} \Delta \tilde{T} + \Delta \tilde{P}$$
(4)

with

$$\Delta \tilde{T} = \tilde{T} + 1 \tag{5}$$

$$\Delta \tilde{\mu} = \tilde{\mu} - \tilde{\mu}_0(\tilde{\tau}) \tag{6}$$

Here $\tilde{P}_0(\tilde{T})$ and $\tilde{\mu}_0(\tilde{T})$ are analytic functions of $\Delta \tilde{T}$, while $\Delta \tilde{P}$ contains the singular, i.e., nonanalytic, contributions to the potential \tilde{P} . The equations for these functions are fully specified in Appendix A. The analytic functions are represented by truncated power series in terms of $\Delta \tilde{T}$ while the singular part $\Delta \tilde{P}$ is related to $\Delta \tilde{\mu}$ and $\Delta \tilde{T}$ with the aid of two auxiliary (parametric) variables *r* and θ . The computer program that generates values of the thermodynamic functions from our fundamental equation has been published elsewhere (10).

The fundamental equation contains the following constants: three critical parameters, P_c , T_c and ρ_c ; three critical exponents, β , δ , and Δ_1 ; five parameters, a, k_0 , k_1 , c, and b^2 , in the singular contribution $\Delta \tilde{P}$; four "background" parameters, \tilde{P}_1 , \tilde{P}_2 , \tilde{P}_3 , and \tilde{P}_{11} , that specify the analytic contributions to \tilde{P} ; and four "background" parameters, $\tilde{\mu}_c$, $\tilde{\mu}_1$, $\tilde{\mu}_2$, and $\tilde{\mu}_3$, that specify the analytic contribution to the thermal properties as a function of temperature. The three critical exponents are universal, i.e., the same for all fluids, and their "best" theoretical values are imposed on the evaluation of the other constants.

The values that we have assigned to the parameters in the fundamental equation for isobutane are listed in Appendix B. The way in which the parameters were determined is the topic of the following section. The equation is valid in the range of temperatures and densities given in eq 2.

Data Sources

The PVT data of Beattie et al. consist of 13 isotherms (12) containing 174 points in the range

$$407.764 \le T \le 408.314$$
 K $180.5 \le \rho \le 270.3$ kg/m³

and data on a number of isotherms at higher temperatures (13). Of these, the 423.170 K isotherm contains six points in the density range 145.2-290.4 kg/m³. The next higher isotherm,



Figure 1. Range of validity of the present formulation is given by the heavy-drawn rectangle in the temperature-density plane. The dotted rectangle indicates the range excluded by Waxman and Gallagher. The hatched region is that in which data points were generated from the Waxman-Gallagher formulation in order to define our surface.

at 448.182 K, is outside the range of validity of our equation.

The following estimates were made of the experimental errors of the data of Beattie et al.:

$$\sigma_{\rho} = 10^{-4} \text{ MPa}$$
 $\sigma_{\tau} = 0.005 \text{ K}$
 $\sigma_{\rho} = 0.058 \text{ kg/m}^3 (0.001 \text{ mol/dm}^3)$ (7)

The mass of the sample was determined by weight, but the data were reported in molar units. Beattie et al. used M = 58.077 g/mol for isobutane and, in order to conserve consistency, we used this same value of *M* to reconvert their density data to units of kg/m³.

For reasons given in the Introduction, we supplemented the experimental data with calculated points generated from the surface of Waxman and Gallagher (6). We generated 215 *PVT* data points on a grid in a region in the ρ -T space bounded, on the sides, by

$$420 \le T \le 438 \text{ K}$$
 $140 \le \rho \le 160 \text{ kg/m}^3$
 $420 \le T \le 438 \text{ K}$ $280 \le \rho \le 300 \text{ kg/m}^3$

and at the top by

$$430 \le T \le 438 \text{ K}$$
 $140 \le \rho \le 300 \text{ kg/m}^3$

This range is indicated in Figure 1. The grid points were spaced by 2 K and 5 kg/m³. The range around the critical point excluded by Waxman and Gallagher, eq 1, is also indicated in Figure 1.

In the fitting procedure, we have assigned the same uncertainties to the generated points as to the experimental *PVT* data. Beattie's temperatures were reported on the International Practical Temperature Scale (IPTS) of 1948. We have converted the experimental temperatures to IPTS of 1968 for the present analysis. The surface of Waxman and Gallagher was assumed to be on IPTS-68. All temperatures reported in what follows will be on IPTS-68 unless a statement to the contrary is made.

Critical-Point Parameters

Beattie et al. obtained the critical parameters of isobutane from their *PVT* data in a range of 0.6 K around T_c by a graphical construction of the coexistence dome (*12*). They obtained

$$T_c = 408.14_4 \text{ K}$$
 $\rho_c = 221 \text{ kg/m}^3$
 $P_c = 3.648 \text{ MPa}$ (8)

It is our contention that this dome was not drawn sufficiently flat. A preliminary analysis of Beattie's data by a simple scaled equation yielded (3)

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$$T_c = 407.865 \text{ K}$$
 $\rho_c = 226.85 \text{ kg/m}^3$
 $P_c = 3.6306 \text{ MPa}$ (9)

Since scaled analyses of *PVT* data do not determine the critical temperature very precisely, one of us (J.M.H.L.S.) determined the critical temperature of 99.98% pure isobutane by observation of the meniscus disappearance, and the critical density by weight (Appendix E). The results are

$$T_{\rm c} = 407.84 \pm 0.02 \, {\rm K}$$
 $\rho_{\rm c} = 225.5 \pm 2 \, {\rm kg/m^3}$ (10)

These values are clearly consistent with those obtained by the simple scaled analysis of Beattie's data. We have therefore, in our present analysis, imposed the observed value of $T_c = 407.84$ K.

If the experimental value of ρ_c , eq 10, is imposed on the fit to the present scaled equation, the reduced χ^2 equals 1.72, compared with a minimum value of 1.26 reached for $\rho_c = 226.42 \text{ kg/m}^3$. We fett that the increase in χ^2 could be tolerated and therefore we have imposed the critical parameter values

$$T_c = 407.84 \text{ K}$$
 $\rho_c = 225.5 \text{ kg/m}^3$ (11)

The critical pressure was treated as an adjustable parameter in the fit to the PVT data.

Equation of State Parameters

The values that we have accepted for the universal parameters β , δ , Δ_1 , and b^2 (Appendix B) reflect the current theoretical knowledge (9) and are the same as the values that we used to represent the thermodynamic properties of light and heavy water (10, 11).

The parameters a, k_0 , k_1 , c in the scaled contribution, and the pressure background parameters \tilde{P}_1 , \tilde{P}_2 , \tilde{P}_3 , \tilde{P}_{11} , are system dependent. These parameters, together with the critical pressure P_c , are determined by fitting the equation of state to the *PVT* data, with the exception of \tilde{P}_{11} , which is determined from the slope of the diameter of the coexistence curve; this slope was deduced from the equation of Waxman et al. to be equal to -0.4971 kg/m^3 , or -0.9011 in reduced units. In our analysis we found that the coefficient \tilde{P}_3 was not statistically significant and did not improve the accuracy of the representation; it was therefore set equal to zero.

The constant \tilde{P}_1 is related to the slope of the vapor pressure curve at the critical point. Our first approach was to estimate this slope by fitting Waxman's new vapor pressure data (6) in the range of 298.15–398.15 K with a scaled equation, while imposing our choices of P_c and T_c . The equation and the results of the fit are summarized in Appendix C. From this fit, we obtained $\tilde{P}_1 = 5.8038$. We realize, however, that the use of a scaled equation in such a large range is not justified. If \tilde{P}_1 is left a free parameter in the fit to Beattie's data, we obtain $\tilde{P}_1 = 5.8858 \pm 0.0015$, a significantly higher value. The low value from the vapor pressure analysis cannot be reconciled with the *PVT* data. It is the high value from the *PVT* data that we have adopted for \tilde{P}_1 .

The values of the parameters of the equation of state, obtained by fitting the PVT data of Beattie et al. plus points generated from the surface of Waxman et al. to our equation, are listed in Appendix B. The reduced χ^2 of the fit is 1.72.

In Figures 2 and 3 we show the pressure deviations of the experimental data of Beattie et al. from our surface. In Figure 3 we also show the deviations of the surface of Waxman et al. from our surface along selected isotherms as indicated by the dashed curves. Most of the Beattie data are fitted to better than 0.002 MPa and the departures of the Waxman surface from our own for temperatures 423 K and higher are also within the 0.002 MPa range.



Figure 2. Departures of the isothermal PVT data of Beattie et al. (12) from our surface (1 kPa = 0.001 MPa = 0.01 bar).



Figure 3. Departures of the *PVT* data of Beattle et al. (12, 13) and of Waxman (6) from our surface along selected isotherms. The curves denote the departures of the Waxman–Gallagher formulation (6) from our surface. All depatures are well within the 0.002-MPa range (1 kPa = 0.001 MPa = 0.01 bar).

Coexistence Curve

The location of the phase boundary turned out to be the most frustrating part of the correlation. Reliable experimental data for the saturation properties are not available for the vapor above 368 K and for the liquid above 396 K. The coexistence curve that we predict is based on Beattie's PVT data which extend over a range of no more than 0.1 K below the critical point. Our coexistence curve ceases to be valid below 405 K. The coexistence curve prediction of Waxman and Gallagher, however, is not valid for temperatures exceeding 401.8 K, eq 1. We have compared with the coexistence curve from the correlation of Goodwin and Haynes (7) which equation incorporates some of the critical anomalies and has its critical point at the physical critical temperature. The comparison is shown in Table I. It is seen that the liquid densities agree on the level of 0.2%, which is excellent. The vapor densities of our equation are up to 1.8% lower than those of Goodwin and Haynes. In the absence of data above 368 K, this is probably not a bad agreement. Even though a "biend" with the Waxman surface has been our goal, we have not tried to readjust our surface in order to match up with Waxman's coexistence curve: doing this would have brought our coexistence curve further from the dome predicted by Goodwin and Haynes and would have put undue strain on our surface in other regions.

We note that classical equations lead to a coexistence dome which is not sufficiently flat (14). As a consequence such equations tend to imply a critical temperature which is too high (15). Indeed, when the analytic equation of Waxman and



Figure 4. In the $T-\rho$ plane, the range is indicated in which specific thermodynamic derivatives from the Waxman–Gallagher surface agree with the present surface to better than 1%: (A) compressibility K_T , (B) specific heat C_ρ , (C) specific heat C_{ν} . The dotted rectangle indicates the range excluded by the Waxman–Gallagher formulation.

Gallagher, valid away from the critical point, is extrapolated into the critical region, it implies values for T_c and P_c about 1.8 K and 0.11 MPa too high.

Thermal Background Parameters

In our analyses of the thermodynamic properties of H₂O and D₂O, we used experimental data on the thermal properties such as specific heats or speed of sound to determine the thermal background parameters $\tilde{\mu}_2$ and $\tilde{\mu}_3$. Since experimental data on the thermal properties of isobutane in the critical region are not available, we used the thermodynamic surface of Waxman et al. to determine the values of the parameters $\tilde{\mu}_2$ and $\tilde{\mu}_3$.

We therefore generated isochoric specific heat, C_v , data from the equation of Waxman et al. in the range shown in Figure 1. After subtracting the scaled contributions to C_v from these generated data, we have fitted the remainder to a linear expression to determine the parameters $\tilde{\mu}_2$ and $\tilde{\mu}_3$.

First, in order to determine whether the inclusion of the background parameter $\tilde{\mu}_3$ significantly improves our surface, we set $\tilde{\mu}_3 = 0$ and fitted the C_v remainder to $\tilde{\mu}_2$. We find $\tilde{\mu}_2 = -37.705 \pm 0.023$. With this value for $\tilde{\mu}_2$, the differences in C_v calculated from our equation and that of Waxman et al.

Table I. Comparison with the Coexistence Dome of Goodwin and Haynes

	isities,							
temp, K	Goodwin	scaled	diff	diff, %				
404.0	315.18	314.60	0.58	0.18				
404.5	310.75	310.10	0.65	0.21				
405.0	305.88	305.19	0.69	0.22				
405.5	300.44	299.77	0.67	0.22				
406.0	294.22	293.61	0.61	0.21				
406.5	286.81	286.36	0.45	0.16				
407.0	277.36	277.19	0.17	0.06				
407.5	263.11	263.43	-0.32	-0.12				
407.8	243.92	244.09	-0.17	-0.07				
saturated vapor densities,								
		kg/m³						
temp, K	Goodwin	scaled	diff	diff, %				
404.0	143.24	140.64	2.60	1.85				
404.5	147.10	144.63	2.47	1.71				
405.0	151.35	149.01	2.34	1.57				
405.5	156.11	153.92	2.19	1.43				
406.0	161.56	159.54	2.02	1.27				
406.5	168.06	166.25	1.81	1.09				
407.0	176.34	174.86	1.48	0.85				
407.5	188.82	188.04	0.78	0.42				
407.8	205.84	206.98	-1.14	-0.55				
Table II	Table II							
	Criti	cal Paramet	ters					

Critical Para	neters
$T_{\rm c} = 407.84 \ {\rm K}^a$	$P_{c} = 3.6290 \text{ MPa}^{b}$
$\rho_{\rm c} = 225.5 \rm kg/m^{3} u, 0$	
Critical Expo	onents
$ \substack{\beta = 0.325^c \\ \delta = 4.82^c } $	$\Delta_1 = 0.50^c$
Parameters in Scali	ng Functions
$a = 22.0163^{b}$	$c = -0.0096833^{b}$
$k_0 = 1.19385^b$	$b^2 = 1.3757^d$
$k_1 = 0.50552^{b}$	
\sim Pressure Backgrour	nd Parameters
$P_{21} = 5.8858^{b}$	$P_{\sim 3} = 0^{b}$
$P_2 = -22.0805^{b}$	$P_{11} = -0.068209^{e}$
Thermal Backgroun	d Parameters
$\widetilde{\mu}_{c} = -4.9535^{f}$	$\widetilde{\mu}_{2} = -32.2295^{g}$
$\widetilde{\mu}_{1}^{T} = -21.6912^{f}$	$\widetilde{\mu}_3 = -33.5271^g$

^a From direct determination. ^b From fit to PVT data.

^c Fixed from theory. ^d Same as for H_2O and D_2O .

^e From the slope of the coexistence curve diameter.

^f From identification of our surface with that of Waxman et al. at T = 438 K and $\rho = 205$ kg/m³. ^g From matching our C_v with that of Waxman et al. in the range shown in Figure 1.

become as much as 8% in the range where both equations claim validity (Figure 1).

Next, with both $\tilde{\mu}_2$ and $\tilde{\mu}_3$ adjustable, we found

$$\tilde{\mu}_2 = -32.230 \pm 0.111$$

 $\tilde{\mu}_3 = -33.527 \pm 0.665$ (12)

With these parameter values the differences in C_v are less than 1% throughout the above range. We therefore conclude that the presence of the parameter $\tilde{\mu}_3$ in the thermal background improves our surface significantly, and we adopt the values for the parameters $\tilde{\mu}_2$ and $\tilde{\mu}_3$ as specified in eq 12. In Figure 4 we show the regions where compressibility K_T and specific heats C_v and C_p of our equation agree with those of Waxman et al. to better than 1%.

In order to complete our equation we need to adopt values for $\tilde{\mu}_c$ and $\tilde{\mu}_1$ which are related to the zero points of entropy and energy. We determine these zero-point constants by

Table III

	temp, K	P _{exptl} , MPa	P _{calcd} , MPa	P _{exptl} – P _{calcd} , MPa
1	298.15	0.3500	0.3501	-0.0001
2	303.15	0.4043	0.4041	0.0002
3	308.15	0.4641	0.4640	0.0001
4	313.15	0.5304	0.5304	0.0000
5	318.15	0.6032	0.6036	-0.0 0 04
6	323.15	0.6836	0.6840	-0.0004
7	328.15	0.7725	0.7720	0.0005
8	333.15	0.8683	0.8682	0.0001
9	333.15	0.8676	0.8682	-0.0006
10	343.15	1.0867	1.0866	0.0001
11	353.15	1.3432	1.3429	0.0003
12	363.15	1.6408	1.6411	-0.0 0 03
13	373.15	1.9855	1.9859	-0.0004
14	383.15	2.3819	2.3821	-0.0 0 02
15	393.15	2.8361	2.8362	-0.0001
16	398.15	3.0879	3.0875	0.0004

Table IV. Coexisting Phase Properties

identifying the energy and entropy of our surface at T = 438 K and $\rho = 205$ kg/m³ with the energy and entropy of the global equation of Waxman and co-workers. At this point the difference in pressures calculated from our equation and from that of Waxman et al. is 0.009%, the difference in specific heat at constant volume is 0.07%, the difference in specific heat at constant pressure is 0.1%, and the difference in compressibility is 0.07%. The condition that the values of the energy and entropy coincide with those calculated from the global surface of Waxman et al. at this point yields

$$\tilde{\mu}_{c} = -4.953$$

 $\tilde{\mu}_{1} = -21.691$ (13)

The reference points of enthalpy and entropy of that correlation are the liquid at the normal boiling point as defined by the surface (T = 261.395 K for P = 0.101325 MPa). This completes the determination of the parameters. A complete listing

****			latent	internal			·····		velocity
	press.,	density,	heat,	energy,	enthalpy,	entropy,	$c_{\nu}, \mathrm{kJ}/$	$c_p, \mathbf{kJ}/$	of sound,
temp, K	MPa	kg/m ³	kJ/kg	kJ/kg	kJ/kg	kJ/(kg K)	(kg K)	(kg K)	m/s
				Lic	nuid				
406.00	3.5186	293.61	68.50	413.9	425.9	1.2407	2.432	19.98	124.8
406.10	3.5245	292.27	67.11	414.7	426.7	1.2426	2.441	21.07	123.6
406.20	3.5304	290.87	65.67	415.4	427.5	1.2446	2.451	22.31	122.4
406.30	3.5363	289.43	64.17	416.2	428.4	1.2466	2.461	23.72	$1\overline{2}1.2$
406.40	3.5423	287.92	62.62	416.9	429.2	1.2487	2.472	25.34	119.9
406.50	3.5482	286.36	61.01	417.7	430.1	1.2508	2.484	27.24	118.6
406.60	3.554 2	284.72	59.32	418.6	431.1	1.2530	2.497	29.47	117.3
406.70	3.5601	283.00	57.55	419.4	432.0	1.2553	2.511	32.13	116.0
406.80	3.5661	281.18	55.69	420.3	433.0	1.2577	2.527	35.36	114.6
406.90	3.5721	279.25	53.72	421.3	434.0	1.2602	2.545	39.36	113.2
407.00	3.5781	277.19	51.61	422.2	435.1	1.2629	2.565	44.42	111.7
407.10	3.5841	274.97	49.35	423.3	436.3	1.2657	2.587	51.02	110.1
407.20	3.5901	272,56	46.90	424.4	437.6	1.2687	2.614	59.94	108.5
407.30	3.5962	269.89	44.19	425.6	438.9	1.2720	2.646	72.61	106.8
407.40	3.6022	266.90	41.16	426.9	440.4	1.2756	2.685	91.87	105.0
407.50	3.0083	203.43	37.00	428.4	442.1	1.2797	2.736	124.21	103.0
407.00	3.0144	209.22	07.04	430.2	444.Z	1.2840	2.809	100.17	100.7
407.70	3.0200	200.00	41.04	432.3	440.0	1.2910	2.920	1796 56	97.0
407.80	3 6290	2225.50	0.00	443.8	459.9	1 3231	0.241	1720.50	92.0
101.01	0.0200	220.00	0.00	110.0	100.0	1.0201			0.0
				Va	apor				
405.00	3.4602	149.01	80.56	476.1	499.3	1.4224	2.507	20.62	120.1
405.10	3.4660	149.95	79.47	475.8	498.9	1.4213	2.513	21.35	119.9
405.20	3.4718	150.90	78.37	475.5	498.5	1.4201	2.520	22.14	119.6
405.30	3.4110 91991	150.00	76.09	475.1	498.0	1.4189	2.527	22.99	119.4
405.40	3 4 8 9 3	153.00	74.89	474.0	497.0	1.4177	2.004	23.92	119.1
405.60	3 4 9 5 1	154.97	73.68	474.0	497.1	1.4104 1 4151	2.542	24.94	118.6
405.70	3,5010	156.06	72.44	473.6	496.1	1.4138	2.558	27.28	118.3
405.80	3,5068	157.18	71.16	473.2	495.6	1.4124	2.567	28.63	118.0
405.90	3.5127	158.34	69.85	472.8	495.0	1.4109	2.576	30.13	117.7
406.00	3.5186	159.54	68.50	472.4	494.4	1.4094	2.585	31.80	117.4
406.10	3.5245	160.78	67.11	471.9	493.8	1.4079	2.595	33.69	117.1
406.20	3.5304	162.06	65.67	471.4	493.2	1.4062	2.606	35.82	116.8
406.30	3.5363	163.40	64.17	470.9	492.6	1.4045	2.617	38.24	116.4
406.40	3.5423	164.79	62.62	470.4	491.9	1.4028	2.630	41.03	116.1
406.50	3.5482	166.25	61.01	469.8	491.1	1.4009	2.643	44.27	115.7
406.60	3.5542	167.78	59.32	469.2	490.4	1.3989	2.657	48.06	115.3
400.70	3.3001	109.39	07.00 55.60	400.0	489.0	1.3908	2.672	52.58	114.9
406.80	3 5791	179.09	53 79	407.9	400.1	1 2020	2.009	28.03 64 74	114.4
407.00	3 5781	174.86	51 61	466.3	486.8	1 3897	2.708	73 18	114.0
407.10	3.5841	176.96	49.35	465.4	485.7	1.3869	2.753	84.09	112.8
407.20	3.5901	179.26	46.90	464.4	484.5	1.3839	2.780	98.72	112.1
407.30	3.5962	181.81	44.19	463.3	483.1	1.3805	2.813	119.26	111.3
407.40	3.6022	184.69	41.16	462.1	481.6	1.3766	2.853	150.03	110.4
407.50	3.6083	188.04	37.65	460.6	479.8	1.3721	2.905	200.80	109.2
407.60	3.6144	192.12	33.42	458.8	477.6	1.3666	2.977	298.76	107.5
407.70	3.6205	197.55	27.84	456.3	474.6	1.3593	3.094	556.28	105.0
407.80	3.6266	206.98	18.33	452.0	469.5	1.3467	3.396	2416.05	99.0
407.84	3.0290	220.5U	0.00	443.8	459.9	1.3231			0.0

KJ/KG KJ/(KG,K)

CP CU VELOCITY PHASE DF Sound Region KJ/(KG.K) M/S

KJ/(KG+K)

			_ <u>.</u>				·							· · · · · · · · · · · · · · · · · · ·	
т	PRESSURE	RHO	INTERNAL	ENTHAL P	FNTROPY	CE	сv		PHASE	Ŧ	PEFESURE	RHD	INTERNAL	ENTHAL P	
	TREBBORE	N/IO	ENERGY					OF SOUND	REGION		TREEBOIRE		ENERGY	ENTRE	
DEG C	MPA	KG/M3	KJ/KG	KJ/KG	KJ/(KG+K)	KJ7()	(6.K)	H/S		DEG C	HF A	KG/H3	KJ/KG	KJ/KG	KJ/(KG,K
405.0	3.4602	150.0	4/0.2	478.3	1.4198		5.049		ź	415.0	3,8652	140.0	477.0	510 4	1.4/94
405.0	3.4602	170.0	459.5	479.9	1.3744		4.900		2	415.0	3.9486	170.0	488.9	512.1	1.4462
405.0	3.4602	180.0	453.0	472.2	1,3555		4.768		2	415.0	3.9791	180.0	483.6	505.9	1.4308
405.0	3.4602	190.0	447.1	465.4	1.3385		4.650		2	415.0	4.0044	190.0	478.9	499.9	1,4161
405.0	3,4602	200.0	441.9	459.2	1.3233		4.043		2	415.0	4.0260	200.0	4/4.1	494.2	1,4020
405.0	3.4602	220.0	432.8	448.5	1.2970		4.359		2	415.0	4.0636	220.0	465.0	483.5	1.3758
405.0	3.4602	230.0	428.8	443.9	1.2855		4,280		2	415.0	4.0821	230.0	460.7	478.5	1.3534
405.0	3.4602	240.0	425.2	439.6	1.2750		4.206		2	415.0	4.1021	240.0	456-5	473.6	1.3515
405.0	3,4602	250.0	421.9	435.7	1.2654		4.139		2	415.0	4.1252	250.0	452.4	468.9	1,3400
405.0	3.4602	270.0	416.0	428.8	1.2482		4.019		2	415.0	4.1983	270.0	444.5	440.0	1.3178
405.0	3.4602	280.0	413.3	425.7	1.2406		3.966		2	415.0	4,2338	280.0	440.5	455.6	1.3070
405.0	3.4602	290.0	410.8	422.8	1.2334		3,916		2	415.0	4.2932	290.0	436.6	451.4	1,2963
404 0	7 5037	150.0	47P A	E01 4	1 4747	17 75	2 470	120.9	•						
	0.000/		4/0/0	50114	1.420/	1/1/3	2.477	12017	•	420.0	4.1217	160.0	504.1	531.9	1.4909
406.0	3,5106	160.0	472.0	494.0	1.4084		5.226		2	420.0	4.1751	170.0	500.9	525.5	1.4750
406.0	3.5186	170.0	464.5	485.2	1.3867		5,067		2	420.0	4.2215	180.0	495.9	519.4	1.4598
406.0	3.5186	180.0	457.8	477.4	1.3674		4,926		2	420.0	4.2625	190.0	491.0	513.5	1.4452
406.0	3,5186	190.0	451.9	470.4	1.3502		4.800		2	420.0	4.2997	200.0	486.3	507.8	1.4313
406.0	3,5186	210.0	441.6	458.4	1.3206		4.584		2	420.0	4.3348	220.0	477.3	497 1	1.41/9
406.0	3,5186	220.0	437.2	453.2	1.3079		4.491		2	420.0	4.4038	230.0	472.9	492.1	1.3924
406.0	3.5186	230.0	433.2	448.5	1.2962		4.405		2	420.0	4.4413	240.0	468.7	487.2	1.3806
406.0	3.5186	240.0	429.5	444.1	1,2855		4.327		2	420.0	4.4832	250.0	464.5	482.4	1.3689
406.0	3.5186	250.0	426.1	440.1	1.2757		4,255		2	420.0	4.5317	260.0	460.4	477.8	1.3575
406.0	3.5186	270.0	420.0	436.0	1.2583		4.129		ź	420.0	4.5895	270.0	450.3	473.3	1,3463
406.0	3.5186	280.0	417.3	429.9	1.2505		4.071		2	420.0	4.7470	290.0	448.3	464.7	1.3243
406.0	3.5186	290.0	414.B	426.9	1.2432		4.017		2						
										425.0	4.2509	150.0	523.1	551.5	1.5354
407.0	3.5450	150.0	480.5	504.1	1.4326	15.13	2.451	122.0	1	425.0	4.3291	160.0	517.9	545.0	1.5189
407.0	3,5751	170.0	469.0	470.0	1.3970	24.22	2.647	115.2	÷	420.0	4.3987	10.0	507.9	538.7	1.5032
407.00	0,0,01	1.010	40/10	47010	1.5//0	40177	2104/		•	425.0	4.5185	190.0	503.1	526.8	1.4737
407.0	3.5781	180.0	462.9	482.8	1.3799		5.253		2	425.0	4.5720	200.0	498.4	521.2	1.4598
407.0	3.5781	190.0	456.8	475.6	1.3623		5.110		2	425.0	4.6236	210.0	493.8	515.8	1.4465
407.0	3,5781	200.0	451.3	469.2	1.3465		4.981		2	425.0	4.6749	220.0	489.3	510.6	1.4336
407.0	3.5781	220.0	441.8	458.1	1.3322		4.759		5	425.0	A. 7840	230.0	480.7	505.5	1.4000
407.0	3,5781	230.0	437.7	453.2	1,3073		4.663		2	425.0	4.8460	250.0	476.5	495.8	1.3972
407.0	3.5781	240.0	433.9	448.8	1.2964		4.574		2	425.0	4.9162	260.0	472.3	491.2	1.3857
407.0	3.5781	250.0	430.4	444.7	1.2864		4.493		2	425.0	4.9976	270.0	468.2	486.7	1.3743
407.0	3.5/81	280.0	427.2	411.0	1.2//2		4.41/		ž	425.0	5.0937	280.0	464.1	482.3	1.3631
-0/.0	3.5/61	27010	42412	43/13	1.2000		4.346		-	425.0	5.2086	290.0	460.0	4/8.0	1.3520
407.0	3.5805	280.0	421.2	434.0	1.2601	34.85	2.525	114.9	1	430.0	4.4400	150.0	534.9	564.5	1.5628
407.0	3.5952	290.0	417.7	430.1	1.2502	18.70	2.425	126.4	1	430.0	4.5342	160.0	529.7	558.1	1.5465
				E04 0	4 4700					430.0	4.6200	170.0	524.7	551.9	1.5309
408.0	3.5859	150.0	482.9	499.7	1.4300	19.57	2.430	119.0	;	430.0	4.8790	180.0	519.8	545.9	1.5160
408.0	3.6232	170.0	471.6	492.9	1.4042	31.60	2.572	116.7	i	430.0	4.8434	200.0	510.4	534.6	1.4879
408.0	3.6316	180.0	466.2	486.4	1.3880	57.33	2.667	113.7	1	430.0	4.9124	210.0	505.8	529.2	1.4745
408.0	3.4359	190.0	461.0	480.1	1.3726	120.13	2.788	110.4	1	430.0	4,9816	220.0	501.3	524.0	1.4617
408.0	3.63//	210.0	456.0	4/4.2	1.3560	270.03	1.101	102.2	1	430.0	5.0531	230.0	476.7	518.9	1.4492
408.0	3.4387	220.0	446.7	463.3	1.3312	1596.97	3.208	98.4	1	430.0	5.2121	250.0	488.4	509.2	1.4251
408.0	3.6389	230.0	442.5	458.3	1.3191	1526.54	3.179	96.7	1	430.0	5.3048	260.0	484.2	504.6	1.4135
408.0	3.6392	240.0	438.5	453.7	1.3078	678.23	3.023	97.7	1	430.0	5.4104	270.0	480.0	500.1	1,4020
408.0	3.6400	250.0	434.7	449.3	1.2970	232.66	2.832	101.1	1	430.0	5.5327	280.0	475.9	495.6	1.3907
408.0	3.6421	220.0	431.0	445.0	1.7763	47.10	2.553	112.9	;	430.0	5.6/58	290.0	4/1./	491.3	1.3795
408.0	3.6586	280.0	423.7	436.8	1.2662	23.74	2.465	121.3	i	435.0	4.6270	150.0	546.6	577.4	1.5899
408.0	3.6794	290.0	420.1	432.8	1.2561	15.34	2.398	131.4	1	435.0	4.7373	160.0	541.5	571.1	1.5738
			ADT -							435.0	4.8395	170.0	536.5	565.0	1.5583
409.0	3.45200	160.0	400.3	502.5	1.4971	16.62	2.449	124.2	1	435.0	4.9352	180.0	531.7	557.1	1.5435
409.0	3.6707	170.0	474.2	495.8	1.4104	24.39	2.527	118.0	ī	435.0	5.1140	200.0	522.3	547.0	1.5155
409.0	3.6823	180.0	468.8	489.3	1.3944	37.62	2.591	115,4	1	435.0	5.2008	210.0	517.B	542.5	1.5022
409.0	3.6896	190.0	463.7	483.1	1.3793	59.59	2.656	112.8	1	435.0	5.2886	220.0	513.3	537.3	1.4893
409.0	3.6941	200.0	458.8	477.3	1.3649	92.53	2.714	110.4	1	435.0	5.3796	230.0	508.9	532.3	1.4768
409.0	3.6993	220.0	449.4	466.4	1.3384	155.72	2.767	106.7	i	430.0	5.5804	240.0	500.3	527.4	1.4646
409.0	3.7013	230.0	445.4	461.5	1.3262	147.59	2.748	106.1	1	435.0	5.6964	260.0	496.1	518.0	1.4409
409.0	3.7037	240.0	441.3	456.8	1.3146	112.40	2.702	106.7	1	435.0	5.8267	270.0	491.9	513.4	1.4294
409.0	3.7071	250.0	437.4	452.3	1.3036	73.61	2.636	108.8	1	435.0	5,9755	280.0	487.7	509.0	1.4180
409.0	3.7126	260.0	433,6	447.9	1,2929	28.37	2.003	118.4	1	435.0	6.1471	290.0	483.5	504.7	1.4047
409.0	3.7383	280.0	424.2	439.5	1.2722	18.73	2.432	126.0	î	438.0	4.7393	150.0	553.4	585.0	1.4040
407.0	3,7648	290.0	422.5	435.4	1,2620	13.25	2.381	135.6	1	438.0	4.8582	160.0	548.6	578.9	1.5900
										438.0	4.9703	170.0	543.7	572.9	1.5746
410.0	3.6668	150.0	487.7	512.2	1.4506	10.92	2.402	125.3	1	438.0	5.0761	180.0	538.8	567.0	1.5598
410.0	3,7177	170.0	474.7	49R.5	1.4165	20.0P	2,494	119.3	i	438.0	5.2750	790.0	520.5	361.4	1.0456
410.0	3.7325	180.0	471.4	492.1	1.4007	28.38	2.544	116.8	1	438.0	5.3738	210.0	524.9	550.5	1.5184
410.0	3.7428	190.0	466.3	486.0	1.3857	40.07	2,589	114.6	1	438.0	5.4729	220.0	520.5	545.3	1.5058
410.0	3.7500	200.0	461.5	480.2	1.3714	54.44	2.625	112.7	1	438.0	5.5758	230.0	516.1	540.3	1.4932
410.0	3.7554	210.0	406.8	4/4.7	1,3450	75.04	2.451	110.3	1	438.0	5.6847	240.0	511.7	535.4	1.4810
410.0	3.7642	230.0	448.1	464.4	1.3328	71.70	2.637	110.1	1	438.0	5.9324	260.0	503.2	526.0	1.4571
410.0	3.7690	240.0	444.0	459.7	1.3211	59.42	2.605	111.0	1	438.0	6.0778	270.0	499.0	521.5	1.4457
410.0	3.7753	250.0	440.0	455.1	1.3099	44.35	2.561	113.2	1	438.0	6.2428	280.0	494.8	517.1	1.4343
410.0	3.7843	260.0	436.2	450.7	1,2991	31.32	2.310	122.4	1	438.0	6.4316	290.0	490.6	512.8	1.4229
410.0	3.8191	280.0	428.4	442.2	1.2781	15.74	2.411	130.0	î						
410.0	3.8511	290.0	424.8	43B.1	1.2678	11.80	2.369	139.3	1						

Table V. Table of Thermodynamic Properties along Isotherms at Regular Density Increments

is given in Appendix B. In Appendix D we give tables of thermodynamic properties of isobutane as derived from our surface.

Discussion

The present formulation supplements that of Waxman and Gallagher (6) in most of the region around the critical point excluded by these authors. In the part of the supercritical range where both formulations claim validity, the agreement is excellent; at given density and temperature pressures agree within 0.002 MPa, enthalples within a few tenths, and entroples within a few thousandths of an SI unit. Discrepancies exist near the phase boundary; neither equation claims validity in the range 401.8-405 K. If both equations are extrapolated to 404 K, the coexisting densities differ by percents, and the enthalpies by a few SI units.

415.0 3.84 415.0 3.91 415.0 3.94 415.0 3.94 415.0 3.94 415.0 4.02 415.0 4.02 415.0 4.04 415.0 4.08 415.0 4.08 415.0 4.12 415.0 4.12	32 150.0 499.6 12 160.0 498.7 12 160.0 488.7 12 180.0 483.6 4 190.0 483.6 4 190.0 474.1 53 210.0 474.1 53 210.0 450.7 21 230.0 465.0 22 250.0 452.4 52 250.0 454.5 52 250.0 454.4 31 260.0 454.4 31 260.0 452.4	525.4 1.479 518.6 1.462 512.1 1.446 505.9 1.430 497.2 1.402 488.8 1.386 483.5 1.375 478.5 1.333 478.6 1.351 468.9 1.340 468.9 1.340 468.9 1.340	4 7,93 2,365 4 9,45 2,393 11,32 2,419 5 13,49 2,441 1 5,80 2,459 0 17,91 2,471 5 19,42 2,476 3 19,95 2,475 5 17,84 2,475 5 17,84 2,453 0 15,74 2,433 1 3,49 2,413 1 4,0 2,780	130.7 1 127.9 1 125.5 1 123.5 1 122.1 1 120.8 1 121.1 1 122.2 1 124.3 1 122.2 1 124.3 1 127.4 1 131.9 1
415.0 4.23 415.0 4.29 420.0 4.05 420.0 4.12 420.0 4.12 420.0 4.22 420.0 4.22 420.0 4.22 420.0 4.24 420.0 4.24 420.0 4.34 420.0 4.34	33 280.0 440.5 32 290.0 434.6 25 150.0 511.4 17 160.0 506.1 15 170.0 500.7 15 190.0 495.9 25 190.0 491.0 77 200.0 481.7 186 210.0 471.0	455.6 1.307 451.4 1.296 538.5 1.507 531.9 1.490 525.5 1.455 519.4 1.455 519.4 1.455 507.6 1.435 507.6 1.431 502.4 1.417 497.1 1.405	9 4.43 2.336 8 2.0 2.343 5 6.49 2.350 7 35 2.369 9 7.35 2.371 9 9.34 2.404 2 10.33 2.415 3 11.16 2.423 11.70 2.424	145.2 1 145.2 1 134.1 1 133.5 1 131.4 1 129.8 1 128.4 1 128.4 1 128.7 1
420.0 4.400 420.0 4.441 420.0 4.483 420.0 4.583 420.0 4.583 420.0 4.583 420.0 4.583 420.0 4.741 425.0 4.755	30 120.0 472.7 31 240.0 468.7 32 250.0 464.5 32 250.0 460.7 32 250.0 460.7 32 250.0 460.7 32 250.0 454.3 35 270.0 452.3 300 280.0 425.3 300 290.0 448.3 307 150.0 523.1 31 140.0 517.9	472.1 1.302 487.2 1.380 487.2 1.380 487.4 1.368 477.6 1.357 473.3 1.346 469.0 1.335 464.7 1.324 551.5 1.5354 545.0 1.516	11.63 2.412 11.63 2.411 10.21 2.399 9 9.27 2.384 5 6.32 2.371 5 6.48 2.345 6 5.64 2.345 6 4.20 2.345	127.7 1 131.5 1 134.2 1 138.0 1 143.1 1 149.4 1 157.0 1 166.1 1
425.0 4.396 425.0 4.461 425.0 4.57 425.0 4.657 425.0 4.627 425.0 4.674 425.0 4.674 425.0 4.727 425.0 4.721 425.0 4.784 425.0 4.916 425.0 4.991	77 170.0 511.8 12 180.0 507.9 15 190.0 503.1 10 200.0 498.4 16 210.0 493.4 19 220.0 489.3 10 200.0 485.0 10 200.0 485.0 10 200.0 485.0 10 240.0 485.0 10 240.0 485.3 10 250.0 476.5 10 250.0 476.5 10 250.0 468.2	530.7 1.5632 532.7 1.4001 526.8 1.4733 521.2 1.4590 515.8 1.4454 510.6 1.4336 505.5 1.4211 500.6 1.4070 495.8 1.3972 491.2 1.3857 486.7 1.3743	 6.80 2.376 7.40 2.388 7.96 2.396 8.41 2.402 8.78 2.404 8.65 2.401 8.34 2.352 7.90 2.387 6.83 2.377 6.83 2.367 	137.2 1 135.9 1 135.3 1 135.3 1 136.0 1 137.5 1 137.5 1 143.1 1 147.4 1 152.8 1
425.0 5.09 425.0 5.206 430.0 4.440 430.0 4.53 430.0 4.620 430.0 4.690 430.0 4.690 430.0 4.690 430.0 4.912 430.0 4.912 430.0 4.912	37 280.0 464.1 36 290.0 460.0 30 150.0 534.9 31 2 460.0 32 12 160.0 529.7 30 170.0 524.7 30 180.0 519.8 31 200.0 515.0 34 200.0 510.4 34 200.0 510.4	482.3 1.3631 478.0 1.3520 564.5 1.5622 558.1 5.545 551.9 1.5305 540.1 1.5160 540.1 1.501 534.6 1.4875 522.2 1.4745 524.0 1.4615	6.30 2.355 5.81 2.344 5.07 2.344 5.89 2.370 6.29 2.370 6.29 2.380 6.45 2.388 6.94 2.393 7.12 2.395 7.12 2.395	167.4 1 176.6 1 146.3 1 144.3 1 142.8 1 141.9 1 141.6 1 141.9 1 143.0 1 144.8 1
430.0 5.053 430.0 5.124 430.0 5.124 430.0 5.304 430.0 5.330 430.0 5.531 430.0 5.532 430.0 5.675 	1 230.0 496.9 1 240.0 492.6 1 250.0 488.4 18 260.0 488.4 18 260.0 484.2 17 280.0 475.7 18 290.0 471.7 19 150.0 546.6 13 160.0 541.5	518.9 1.4492 514.0 1.4370 509.2 1.4251 504.6 1.4135 500.1 1.4020 495.6 1.3907 491.3 1.3795 577.4 1.5899 571.1 1.5738	2 7.10 2.393 6.91 2.389 6.64 2.383 6.31 2.376 5.95 2.368 5.60 2.360 5.26 2.351 4.68 2.344 4.98 2.357	147.6 1 151.3 1 156.0 1 161.8 1 168.7 1 176.9 1 186.2 1 151.3 1 149.6 1
435.0 4.935 435.0 5.026 435.0 5.114 435.0 5.200 435.0 5.200 435.0 5.326 435.0 5.376 435.0 5.476 435.0 5.476 435.0 5.476 435.0 5.476 435.0 5.476	31 170.0 531.7 180.0 531.7 531.7 190.0 527.0 522.3 182 210.0 517.8 162 220.0 513.3 162 230.0 508.9 102 240.0 504.6 162 250.0 500.3 162 270.0 491.9 17 270.0 491.9	559,1 1,5383 553,4 1,5292 547,9 1,5105 542,5 1,5022 537,3 1,4893 532,3 1,4705 527,4 1,4646 527,4 1,4646 522,6 1,4527 518,0 1,4409 513,4 1,4294	5.28 2.30 5.63 2.337 5.63 2.384 6.04 2.389 6.16 2.391 6.16 2.391 6.13 2.387 5.62 2.381 5.62 2.372 5.65 2.372 5.37 2.372	148.4 1 147.7 1 148.3 1 149.7 1 151.9 1 155.0 1 159.0 1 164.0 1 170.1 1 177.4 1
435.0 6.147 438.0 4.738 438.0 4.858 438.0 5.074 438.0 5.177 438.0 5.177 438.0 5.275 438.0 5.373 438.0 5.373 438.0 5.373	1 290.0 483.5 3 150.0 553.6 2 160.0 548.6 3 170.0 548.6 3 170.0 538.8 4 190.0 534.1 98 200.0 529.5 8 210.0 524.9 9 220.0 520.5	504.7 1.4160 508.7 1.4007 578.9 1.5900 577.9 1.5746 567.0 1.5576 561.4 1.5456 555.9 1.5319 550.5 1.5186 545.3 1.5058	4.49 2.359 4.49 2.359 5.01 2.369 5.26 2.376 5.47 2.383 5.44 2.387 5.75 2.390 5.79 2.391	195.2 1 154.3 1 152.7 1 151.6 1 151.3 1 152.1 1 153.6 1 153.6 1 153.6 1
438.0 5.684 438.0 5.684 438.0 5.802 438.0 5.932 438.0 6.077 438.0 6.242 438.0 6.431	240.0 518.1 7 240.0 511.7 6 250.0 507.4 4 260.0 503.2 8 270.0 499.0 8 280.0 494.8 6 290.0 490.6	540,3 1,4932 535,4 1,4810 530,7 1,4690 526,0 1,4573 521,5 1,4457 517,1 1,4343 512,8 1,4229	5.75 2.390 5.65 2.387 5.50 2.384 5.32 2.380 5.11 2.375 4.90 2.369 4.69 2.363	157.3 1 163.5 1 168.7 1 175.0 1 162.3 1 190.7 1 200.3 1

We have refrained from comparing with earlier formulations constructed prior to the availability of the new data. The only other correlation making use of the expanded data base is that of Goodwin and Haynes (7). As mentioned, our coexistence curve agrees with theirs about as well as might be hoped for, given the absence of experimental saturation data above 400 K. In the supercritical range, however, the pressures of the Goodwin-Haynes correlation differ from the Beattle data, and therefore from our surface and from that of Waxman, by substantial amounts ranging, at 423 K, from +0.01 MPa at 116 kg/m³, to +0.08 MPa at 290 kg/m³.

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Appendix A

Revised and Extended Scaling Equations for the Thermodynamic Properties of Fluids.

Reduced Thermodynamic Quantities:

$$\begin{split} \tilde{T} &= -\frac{T_{c}}{T} \qquad \tilde{\mu} = \frac{\mu}{T} \frac{\rho_{c} T_{c}}{P_{c}} \qquad \tilde{P} = \frac{P}{T} \frac{T_{c}}{P_{c}} \\ \tilde{\rho} &= \frac{\rho}{\rho_{c}} \qquad \tilde{U} = \frac{U}{V} \frac{1}{P_{c}} \qquad \tilde{S} = \frac{S}{V} \frac{T_{c}}{P_{c}} \\ \tilde{A} &= \frac{A}{VT} \frac{T_{c}}{P_{c}} \qquad \tilde{H} = \frac{H}{VT} \frac{T_{c}}{P_{c}} \qquad \tilde{\chi}_{T} = \left(\frac{\partial \tilde{\rho}}{\partial \tilde{\mu}}\right)_{T} \\ \tilde{C}_{v} &= \frac{C_{v}}{V} \frac{T_{c}}{P_{c}} \qquad \tilde{C}_{P} = \frac{C_{p}}{V} \frac{T_{c}}{P_{c}} \qquad (A.1) \end{split}$$

(*T* is temperature, μ is chemical potential, *P* is pressure, ρ is density, *U* is energy, *S* is entropy, *A* is Helmholtz free energy, *H* is enthalpy, *V* is volume, C_v is heat capacity at constant *V*, C_p is heat capacity at constant *P*).

Thermodynamic Relations :

$$d\tilde{P} = \tilde{U} d\tilde{T} + \tilde{\rho} d\tilde{\mu}$$

$$d\tilde{A} = -\tilde{U} d\tilde{T} + \tilde{\mu} d\tilde{\rho}$$

$$d\tilde{H} = -\tilde{T} d\tilde{U} + \tilde{\rho} d\tilde{\mu}$$

$$d\tilde{S} = -\tilde{T} d\tilde{U} - \tilde{\mu} d\tilde{\rho}$$
(A.2)

with

$$\begin{split} \tilde{A} &= \tilde{\rho}\tilde{\mu} - \tilde{P} \\ \tilde{H} &= \tilde{P} - \tilde{T}\tilde{U} \\ \tilde{S} &= \tilde{H} - \tilde{\rho}\tilde{\mu} = -\tilde{T}\tilde{U} - \tilde{A} \end{split} \tag{A.3}$$

Fundamental Equations :

$$\Delta \tilde{T} = \tilde{T} + 1 \tag{A.4a}$$

$$\Delta \tilde{\mu} = \tilde{\mu} - \tilde{\mu}_{0}(\tilde{\tau}) \tag{A.4b}$$

$$\tilde{P} = \tilde{P}_{0}(\tilde{T}) + \Delta \tilde{\mu} + \tilde{P}_{11} \Delta \tilde{\mu} \Delta \tilde{T} + \Delta \tilde{P}$$
(A.5)

with

$$\tilde{\mu}_{0}(\tilde{T}) = \tilde{\mu}_{c} + \sum_{j=1}^{3} \tilde{\mu}_{j}(\Delta \tilde{T})^{j}$$
(A.6a)

$$\tilde{P}_{0}(\tilde{T}) = 1 + \sum_{j=1}^{3} \tilde{P}_{j}(\Delta \tilde{T})^{j}$$
(A.6b)

Derived Thermodynamic Quantities:

$$\tilde{\rho} = 1 + \tilde{P}_{11}\Delta\tilde{T} + (\partial\Delta\tilde{P}/\partial\Delta\tilde{\mu})_{\Delta\tilde{T}}$$
(A.7)

$$\tilde{U} = \frac{d\tilde{P}_{0}}{d\tilde{\tau}} - \tilde{\rho}\frac{d\tilde{\mu}_{0}}{d\tilde{\tau}} + \tilde{P}_{11}\Delta\tilde{\mu} + \left(\frac{\partial\Delta\tilde{P}}{\partial\Delta\tilde{\tau}}\right)_{\Delta\tilde{\mu}}$$
(A.8)

$$\tilde{\chi}_{\tau} = (\partial^2 \Delta \tilde{P} / \partial \Delta \tilde{\mu}^2)_{\Delta \tilde{\tau}}$$
(A.9)

$$\begin{pmatrix} \frac{\partial \tilde{P}}{\partial \tilde{T}} \end{pmatrix}_{\tilde{P}} = \\ \frac{d\tilde{P}_{0}}{d\tilde{T}} + \tilde{P}_{11} \left[\Delta \tilde{\mu} - \frac{\tilde{P}}{\tilde{\chi}_{T}} \right] + \left(\frac{\partial \Delta \tilde{P}}{\partial \Delta \tilde{T}} \right)_{\Delta \tilde{\mu}} - \frac{\tilde{P}}{\tilde{\chi}_{T}} \frac{\partial^{2} \Delta \tilde{P}}{\partial \Delta \tilde{\mu} \partial \Delta \tilde{T}}$$
(A.10)

$$\frac{\tilde{C}_{\nu}}{\tilde{\tau}^{2}} = \frac{d^{2}\tilde{P}_{0}}{d\tilde{\tau}^{2}} - \tilde{\rho}\frac{d^{2}\tilde{\mu}_{0}}{d\tilde{\tau}^{2}} - \frac{\tilde{P}_{11}^{2}}{\tilde{\chi}_{\tau}} + \left(\frac{\partial^{2}\Delta\tilde{P}}{\partial\Delta\tilde{\tau}^{2}}\right)_{\Delta\tilde{\mu}} - \frac{2\tilde{P}_{11}}{\tilde{\chi}_{\tau}}\frac{\partial^{2}\Delta\tilde{P}}{\partial\Delta\tilde{\mu}\partial\Delta\tilde{\tau}} - \frac{1}{\tilde{\chi}_{\tau}}\left(\frac{\partial^{2}\Delta\tilde{P}}{\partial\Delta\tilde{\mu}\partial\Delta\tilde{\tau}}\right)^{2} (A.11)$$

$$\tilde{C}_{p} = \tilde{C}_{v} + \frac{\tilde{\chi}_{r}}{\tilde{\rho}^{2}} \left[\tilde{P} - \tilde{T} \left(\frac{\partial \tilde{P}}{\partial \tilde{T}} \right)_{\tilde{\rho}} \right]^{2}$$
(A.12)

Critical Exponents:

$$\begin{aligned} \alpha_0 &= \alpha & \alpha_1 &= \alpha - \Delta_1 \\ \beta_0 &= \beta & \beta_1 &= \beta + \Delta_1 \\ \gamma_0 &= \gamma & \gamma_1 &= \gamma - \Delta_1 \end{aligned}$$
 (A.13)

with

$$2 - \alpha = \beta(\delta + 1) \qquad \gamma = \beta(\delta - 1) \qquad (A.14)$$

Parametric Equations for Singular Terms:

$$\Delta \tilde{\mu} = r^{\beta \delta} a \,\theta (1 - \theta^2) \tag{A.15}$$

$$\Delta \tilde{T} = r(1 - b^2 \theta^2) - c \Delta \tilde{\mu}$$
 (A.16)

$$\Delta \tilde{P} = \sum_{i=0}^{1} r^{2-\alpha_i} a k_i p_i(\theta)$$
 (A.17)

$$(\partial \Delta \tilde{P} / \partial \Delta \tilde{\mu})_{\Delta \tilde{\tau}} = \sum_{i=0}^{1} \left[r^{\beta_i} k_i \theta + c r^{1-\alpha_i} a k_i s_i(\theta) \right] \quad (A.18)$$

$$(\partial \Delta \tilde{P} / \partial \Delta \tilde{T})_{\Delta \tilde{\mu}} = \sum_{i=0}^{1} r^{1-\alpha_i} a k_i s_i(\theta)$$
 (A.19)

$$(\partial^{2}\Delta\tilde{P}/\partial\Delta\tilde{\mu}^{2})_{\Delta\tilde{T}} = \sum_{i=0}^{1} \left[r^{-\gamma_{i}} \frac{k_{i}}{a} u_{i}(\theta) + 2cr^{\beta_{i}-1}k_{i}v_{i}(\theta) + c^{2}r^{-\alpha_{i}}ak_{i}w_{i}(\theta) \right] (A.20)$$

$$\frac{\partial^2 \Delta \tilde{P}}{\partial \Delta \tilde{\mu} \Delta \tilde{T}} = \sum_{i=0}^{1} \left[r^{\beta_i - 1} k_i v_i(\theta) + c r^{-\alpha_i} a k_i w_i(\theta) \right] \quad (A.21)$$

$$(\partial^2 \Delta \tilde{P} / \partial \Delta \tilde{T}^2)_{\Delta \tilde{\mu}} = \sum_{i=0}^{1} r^{-\alpha_i} a k_i w_i(\theta)$$
 (A.22)

Auxiliary Functions:

$$p_i(\theta) = p_{0i} + p_{2i}\theta^2 + p_{4i}\theta^4$$
 (A.23)

$$s_i(\theta) = s_{0i} + s_{2i}\theta^2$$
 $s_i'(\theta) = 2s_{2i}\theta$ (A.24)

$$q(\theta) = 1 + \{b^2(2\beta\delta - 1) - 3\}\theta^2 - b^2(2\beta\delta - 3)\theta^4$$
 (A.25)

$$u_{i}(\theta) = \left[1 - b^{2}(1 - 2\beta_{i})\theta^{2}\right]/q(\theta)$$
 (A.26)

$$v_i(\theta) = \left[\beta_i(1-3\theta^2)\theta - \beta\delta(1-\theta^2)\theta\right]/q(\theta) \quad (A.27)$$

$$\mathbf{w}_{i}(\theta) = \left[(1 - \alpha_{i})(1 - 3\theta^{2})s_{i}(\theta) - \beta\delta(1 - \theta^{2})\theta s_{i}'(\theta) \right] / q(\theta)$$
(A.28)

with

$$p_{0i} = + \frac{\beta \delta - 3\beta_i - b^2 \alpha_i \gamma_i}{2b^4 (2 - \alpha_i)(1 - \alpha_i)\alpha_i}$$

$$p_{2i} = - \frac{\beta \delta - 3\beta_i - b^2 \alpha_i (2\beta \delta - 1)}{2b^2 (1 - \alpha_i)\alpha_i}$$

$$p_{4i} = + \frac{2\beta \delta - 3}{2\alpha_i} \qquad (A.29)$$

$$s_{0i} = (2 - \alpha_i)p_{0i}$$

$$s_{2i} = -\frac{\beta \delta - 3\beta_i}{2b^2 \alpha_i}$$
(A.30)

Two-Phase Properties:

$$\theta = \pm 1$$

 $\Delta \tilde{\mu} = 0$
 $\Delta \tilde{T} = r(1 - b^2)$ (A.31)

vapor pressure

$$\tilde{P}_{vap} = \tilde{P}_{0}(\tilde{T}) + \sum_{i=0}^{1} r^{2-\alpha_{i}} a k_{i} p_{i}(1)$$
 (A.32)

coexisting densities

$$(\tilde{\rho}_{L} + \tilde{\rho}_{V})/2 = 1 + \tilde{P}_{11}\Delta\tilde{T} + \sum_{i=0}^{1} cr^{1-\alpha_{i}}ak_{i}s_{i}(1)$$
$$(\tilde{\rho}_{L} - \tilde{\rho}_{V})/2 = \sum_{i=0}^{1} r^{\beta_{i}}k_{i}$$
(A.33)

Helmholtz free energy

$$\tilde{A} = \tilde{\rho}\tilde{\mu}_{0}(\tilde{T}) - \tilde{P}_{0}(\tilde{T}) - \sum_{i=0}^{1} r^{2-\alpha_{i}}ak_{i}p_{i}(1)$$
(A.34)

energy

$$\tilde{U} = \frac{d\tilde{P}_{0}}{d\tilde{T}} - \tilde{p}\frac{d\tilde{\mu}_{0}(\tilde{T})}{d\tilde{T}} + \frac{1}{1-b^{2}}\sum_{i=0}^{1}(2-\alpha_{i})r^{1-\alpha_{i}}ak_{i}p_{i}(1)$$
(A.35)

entropy

$$\tilde{S} = -\tilde{\rho}\tilde{\mu}_{0}(\tilde{T}) + \tilde{P}_{0}(\tilde{T}) - \tilde{T}\left[\frac{d\tilde{P}_{0}}{d\tilde{T}} - \tilde{\rho}\frac{d\tilde{\mu}_{0}}{d\tilde{T}}\right] + \sum_{i=0}^{1} r^{2-\alpha_{i}}ak_{i}p_{i}(1) - \frac{\tilde{T}}{1-b^{2}}\sum_{i=0}^{1} (2-\alpha_{i})r^{1-\alpha_{i}}ak_{i}p_{i}(1)$$
(A.36)

specific heat C_{ν}

$$\frac{\tilde{C}_{v}}{\tilde{\tau}^{2}} = \frac{d^{2}\tilde{P}_{0}}{d\tilde{\tau}^{2}} - \tilde{\rho}\frac{d^{2}\tilde{\mu}_{0}}{d\tilde{\tau}^{2}} + \left(\frac{1}{1-b^{2}}\right)^{2}\sum_{i=0}^{1}(2-\alpha_{i})(1-\alpha_{i})r^{-\alpha_{i}}ak_{i}p_{i}(1)$$
(A.37)

Appendix B

Parameter values are listed in Table II.

Appendix C

Vapor Pressure of Isobutane. The vapor pressure data of Waxman (5) in the range 298-398 K were fitted to the simple scaled equation

$$P^* = 1 + A_1 \Delta T^* + A^{-} (\Delta T^*)^{2-\alpha} + A_2 (\Delta T^*)^2 + A_3 (\Delta T^*)^3$$
(C.1)

where $P^* = P/P_c$, $\Delta T^* = (T_c - T)/T_c$ and the critical exponent α = 0.1085. Choosing T_c = 407.84 K, P_c = 3.6290 MPa, we obtain $A_1 = -6.8038$, $A^- = 21.5688$, $A_2 = -10.1751$, A_3 = -7.0260 and the deviations listed in Table III.

This fit corresponds with a value of \tilde{P}_1 of 5.8038. Retaining the form of the vapor pressure equation, eq C.1 and the choice of T_c , we can obtain higher values of \tilde{P}_1 only by raising P_c . We would have to raise Pc by as much as 0.07 MPa to obtain a value $\tilde{P}_1 = 5.88$ consistent with Beattle's PVT data. This choice of Pc, however, would be quite inconsistent with Beattie's and Waxman's supercritical PVT data.

Appendix D

Tables of Thermodynamic Properties. In Table IV we list the values of the thermodynamic properties of isobutane along the coexistence curve on the liquid and vapor sides as a function of temperature. In Table V we have tabulated the thermodynamic properties along isotherms at regular density increments.

Appendix E

Measurement of the Critical Density and Temperature of Isobutane. The critical temperature and density of isobutane were determined by observation of the disappearance of the meniscus in the center of an optical cell. The cell was formed by clamping a 316 stainless-steel ring of i.d. 25.4 mm, o.d. 35 mm, and thickness 12.7 mm between two sapphire disks of o.d. 35 mm and thickness 6 mm, with tin foil of 0.025-mm thickness serving as a gasket. A steel capillary with an o.d. of 1.6 mm was welded into the steel ring and connected to a pressure valve. The volume of the cell was calculated from its dimensions to be 6.448 cm³ at room temperature. The cell volume was corrected for the volume of the line and valve (+0.022 cm³) and that of a small magnetic bar (-0.123 cm³) which was used as a stirrer. The volume of the cell at higher temperatures was calculated by using the value 16.5×10^{-6} /K for the average coefficient of linear thermal expansion of the steel ring for temperatures between room temperature and 408 K.

The cell was filled with a sample of isobutane from the same research-grade supply used by Waxman for his PVT measurements (6) and certified by the supplier to be at least 99.9% pure. The amount of isobutane was determined by weighing the cell before and after filling it and was chosen such that the density exceeded the critical density by about 8%. The weighings were done on an analytical balance with a precision to within 0.5 mg.

The cell assembly was immersed in a commercial regulated bath which was provided with windows and filled with high-viscosity silicone oil. The temperature was controlled to ± 0.01 K and measured by a platinum resistance thermometer and a 7-decade Mueller bridge. The resistance thermometer had been calibrated at NBS and its indication at the water triple point was monitored during the experiments.

The bath was heated and the meniscus was observed to disappear at the top of the cell. Small amounts of isobutane were subsequently released and trapped above water inside an inverted graduated glass. An account was kept of the amounts of isobutane released (in 15 steps, from 8% above to 8% below the critical density). The critical temperature and density were taken as those corresponding to the case where the meniscus disappeared in the center of the cell. At the end of the experiments the cell was weighed again. The weight loss was found to be 230 mg-it differed from the loss calculated from the volumes released by 15 mg. Since the weight of the critical sample was 1.435 g, we estimate it to be known to better than 15 mg or 1%.

For the seven different fill densities at which the meniscus disappeared at some level inside the cell, the measured temperatures of meniscus disappearance varied from 407.83 to 407.85 K.

Thus, we conclude that $T_{\rm c}$ = 407.84 \pm 0.02 K and $\rho_{\rm c}$ = $225.5 \pm 2 \text{ kg/m}^3$.

Thermodynamic Properties

- Ρ pressure
- P_c T critical pressure
- temperature
- critical temperature T_c

V	volume
V _c	critical volume
ρ	density
$\rho_{\rm c}$	critical density
μ	chemical potential
A	Helmholtz free energy
Н	enthalpy
U	energy
S	entropy
Kτ	isothermal compressibility
C _p	specific heat at constant pressure
Ć,	specific heat at constant volume
М	molecular weight, $M = 0.0581243$ kg/mol
R	gas constant, R = 143.045 J/(kg K)
σ_{p}	experimental error in the pressure
στ	experimental error in the temperature
$\sigma_{ ho}$	experimental error in the density

Reduced Thermodynamic Properties

Ĩ reduced pressure, $PT_c/(P_cT)$ $\Delta \tilde{P}$ singular part of P Ĩ reduced temperature, $-T_c/T$ ΔĨ \tilde{T} + 1 õ reduced density, ρ/ρ_c reduced chemical potential, $\mu \rho_c T_c / (P_c T)$ μ $\tilde{\mu}_0(\tilde{T})$ chemical potential on the saturation curve and its analytic continuation ƈ Ĥ Ũ Š XĈŶ $\tilde{\mu} = \tilde{\mu}_0(\tilde{T})$ reduced Helmholtz free energy density, AT c/(VTP c) reduced enthalpy density, $HT_c/(VTP_c)$ reduced energy density, $U/(VP_c)$ reduced entropy density, ST c/(VP c) reduced susceptibility, $K_T V_c^2 P_c T / (V^2 T_c)$ reduced specific heat density, $C_v T_c / (VP_c)$ reduced specific heat density $C_p T_c / (VP_c)$

Critical Exponents

critical exponent for the specific heat $\alpha \equiv \alpha_0$ $\beta \equiv \beta_0$ critical exponent for the coexistence curve $\gamma \blacksquare \gamma_0$ critical exponent for the compressibility δ critical exponent for the critical isotherm gap exponent for first Wegner correction Δ_1 α_1 $\alpha_0 - \Delta_1$ $\beta_0 + \Delta_1$ β_1 $\gamma_0 - \Delta_1$ γ_1

Parametric Scaled Equation

r parametric dis	stance variable
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- A parametric contour variable
- a, k₀, constants in scaled equation
- k₁, c, b²

analytic part of the vapor pressure equation

coefficients of $\tilde{P}_{0}(\tilde{T})$ written as a polynomial in \tilde{T}

 $\tilde{P}_{1}, \tilde{P}_{2}, \tilde{P}_{3}$ coefficient of the term $(\Delta \tilde{\mu})(\Delta \tilde{T})$ in the expression for P

coefficients of $\tilde{\mu}_0(\tilde{T})$ as a polynomial in \tilde{T} $\mu_1, \tilde{\mu}_2,$

 $\tilde{\mu}_3$ $p_i(\theta),$ polynomials in θ , i = 0, 1

$$s_i(\theta),$$

 $w_i(\theta)$

 $\tilde{P}_0(\tilde{T})$

P̃ 11

 $q_i(\theta)$ ratios of polynomials in θ , i = 0, 1 $u_i(\theta),$ $v_i(\theta).$

coefficients of the polynomials $p_i(\theta)$ $p_{0i}, p_{2i},$

P 41 coefficients of the polynomials $s_i(\theta)$ s_{0i}, s_{2i}

Registry No. Isobutane, 75-28-5.

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